

July 15, 2016

The Board of Commissioners of Public Utilities
Prince Charles Building
120 Torbay Road, P.O. Box 21040
St. John's, NL A1A 5B2

Attention: Ms. Cheryl Blundon
Director Corporate Services & Board Secretary

Dear Ms. Blundon:

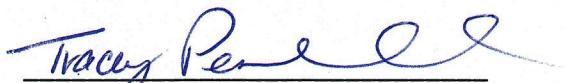
Re: Newfoundland and Labrador Hydro - The Board's Investigation and Hearing into Supply Issues and Power Outages on the Island Interconnected System – Rolling 12 month performance of Hydro's generating units

In accordance with item 2.8 of the Liberty Report Recommendations dated December 17, 2014, please find attached the original plus 12 copies of the quarterly report *Rolling 12 Month Performance of Hydro's Generating Units*.

We trust the foregoing is satisfactory. If you have any questions or comments, please contact the undersigned.

Yours truly,

NEWFOUNDLAND AND LABRADOR HYDRO



Tracey L. Pennell
Senior Counsel, Regulatory

TLP/bs

cc: Gerard Hayes – Newfoundland Power
Paul Coxworthy – Stewart McKelvey Stirling Scales
Sheryl Nisenbaum – Praxair Canada Inc.
ecc: Roberta Frampton Benefiel – Grand Riverkeeper Labrador

Thomas Johnson – Consumer Advocate
Thomas O' Reilly – Cox & Palmer
Danny Dumaresque

**A REPORT TO
THE BOARD OF COMMISSIONERS OF PUBLIC UTILITIES**

**QUARTERLY REPORT
ON
PERFORMANCE OF GENERATING UNITS
FOR THE QUARTER ENDED JUNE 30, 2016**

NEWFOUNDLAND AND LABRADOR HYDRO

JULY 15, 2016



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1 **1.0 Introduction**

2 In this report, Newfoundland and Labrador Hydro (Hydro) provides data on forced outage
3 rates of its generating facilities. This data is provided in relation to historical forced outage
4 rates and as well as in relation to assumptions used in Loss of Load Hours (LOLH) calculations
5 for system planning purposes.

6
7 The forced outage rates are provided for individual generating units at hydraulic facilities,
8 the three units at the Holyrood Thermal Generating Station (HTGS), and Hydro's gas turbines
9 for the current 12-month reporting period of July 1, 2015 to June 30, 2016. The report also
10 provides, for comparison purposes, the individual generating unit data on forced outage
11 rates for the previous period July 1, 2014 to June 30, 2015. Further, total asset class data is
12 presented on an annual basis for the years 2005-2014. This report provides data on outage
13 rates for forced outages, not planned outages.

14
15 The forced outage rates of Hydro's generating units are presented using two measures:
16 Derated Adjusted Forced Outage Rate (DAFOR) for the hydraulic and thermal units and
17 Utilization Forced Outage Probability (UFOP) for the gas turbines.

18
19 Derated Adjusted Forced Outage Rate (DAFOR) is a metric that measures the percentage of
20 the time that a unit or group of units is unable to generate at its maximum continuous rating
21 (MCR) due to forced outages. The DAFOR for each unit is weighted to reflect differences in
22 generating unit sizes in order to provide a company total and reflect the relative impact a
23 unit's performance has on overall generating performance. This measure is applied to
24 hydraulic and thermal units; however, this measure is not applicable to gas turbines because
25 of their nature as a standby unit and relatively low operating hours.

26
27 Utilization Forced Outage Probability (UFOP) is a metric that measures the percentage of
28 time that a unit or group of units will encounter a forced outage and not be available when
29 required. This metric is used for the gas turbines.

1 Included in the forced outage rates are outages that remove the unit from service
2 completely, as well as instances when units are de-rated. If a unit's output is reduced by
3 more than 2%, the unit is considered de-rated by Canadian Electricity Association (CEA)
4 guidelines. Per CEA guidelines, to take into account the de-rated levels of a generating unit,
5 the operating time at the de-rated level is converted into an equivalent outage time.

6

7 In addition to forced outage rates, this report provides outage details for those outages that
8 contributed materially to forced outage rates exceeding those used in Hydro's generation
9 planning analysis.

1 **2.0 Period Ending June 30, 2016 Overview**

Class of Units	July 1, 2014 to June 30, 2015 (%)	July 1, 2015 to June 30, 2016 (%)	Base Planning Assumption (%)
Hydraulic (DAFOR)	2.85	2.15	0.90
Thermal (DAFOR)	10.06	19.45	9.64
Gas Turbine (Combined) (UFOP)	21.19	5.54	10.62
Gas Turbine (Holyrood) (UFOP)	1.56 ¹	2.53	5.00

2

3 The hydraulic DAFOR and the combined² gas turbine UFOP performance (in table above) all
 4 show improvement for the current period, the 12-month period ending June 2016 compared
 5 to the previous period, the 12-month period ending June 2015. There was a decline in
 6 Thermal DAFOR performance for the current period compared to the previous period.

7

8 In the 10 year period prior to 2014, the hydraulic units show a somewhat consistent DAFOR.
 9 The DAFOR of the current 12-month period compared to the previous 10 years is higher,
 10 primarily due to vibration problems experienced at Unit 1 at Bay d’Espoir.

11

12 The thermal units, in the 10 year period prior to 2014, exhibit more variability in DAFOR than
 13 the hydraulic units, but in many years were close to a consistent rate of approximately 10%.
 14 The forced outage rate of the current period ending June 2016 is 19.45% which is above the
 15 base planning assumption of 9.64%, and the sensitivity of 11.64%. This is primarily caused by
 16 an airflow derating on Unit 1 and boiler tube failures on Units 1 and 2.

17

18 Hydro’s combined gas turbines’ UFOP in the 10 year period prior to 2014 was generally
 19 consistent at approximately 10% until the year 2012 when the rate exceeded 50%. Since

¹ Only includes data from March 1, 2015 to June 30, 2015

² Combined Gas Turbines include the Hardwoods, Happy Valley, and Stephenville units. The performance of the Holyrood CT was not included in the combined base planning or sensitivity numbers as these numbers were set prior to the Holyrood CT’s in service date.

1 2012, the UFOP has been improving each year. For the current 12-month period ending June
2 30, 2016, performance was mainly affected by the forced outages to the Happy Valley unit.
3 The decline in performance for the Holyrood CT is related to the data collection period.
4 Performance data for the Holyrood CT for the 12-month period ending June 2015 includes
5 four months of data where the 12-month period ending June 2016 includes a full year of
6 data.
7
8 Note that the data in the charts for 2004 to 2014 are annual numbers (January 1 to
9 December 31), while the data for June 2015 and June 2016 are 12-month rolling (July 1 to
10 June 30 for each period).

1 **3.0 Generation Planning Assumptions**

2 The DAFOR and UFOP indicators used in Hydro’s generation planning model are
3 representative of a historic average of the actual performance of these units. These numbers
4 are noted in the table below under the column “Base Planning Assumption”³.

5
6 Hydro also provides a sensitivity number for DAFOR and UFOP as part of its generation
7 planning analysis. This number takes into account a higher level of unavailability, should it
8 occur, to assess the impact of higher unavailability of these units on overall generation
9 requirements. During the 12-month period ending June 30, 2016, the gas turbine units
10 performed well within this sensitivity range for UFOP. Both the hydraulic and thermal classes
11 performed well outside of the sensitivity range for DAFOR. As part of the ongoing risk review
12 considering energy supply up to Lower Churchill interconnection, Hydro is considering
13 several years of data of DAFOR and UFOP and the resulting implication for meeting reliability
14 criteria.

15
16 The new gas turbine (Holyrood CT) has a lower expected rate of unavailability than the
17 original gas turbines, of 5% compared to 10.62% respectively, due to the fact that the unit is
18 new and can be expected to have better availability than the older units.⁴

³ Hydro is currently completing a risk assessment on thermal generation supply for the period up to interconnection with Labrador and Nova Scotia. As part of this risk assessment, Hydro is reviewing the recent availability results. The outcome of this review may reflect a new base planning assumption for various generation sources.

⁴ Hydro selected a 5% UFOP for the new Holyrood CT following commentary on forced outage rates contained in the *Independent Supply Decision Review – Navigant (September 14, 2011)*

- 1 Hydro's current generation planning assumptions for DAFOR and UFOP are:
- 2

	DAFOR (%)		UFOP (%)	
	Base Planning Assumption	Sensitivity	Base Planning Assumption	Sensitivity
Hydraulic Units	0.90	0.90		
Thermal Units	9.64	11.64		
Gas Turbines - Existing			10.62	20.62
Gas Turbines - New			5.0	10.0 ⁵

⁵ In previous reports this sensitivity value was reported as 5.0%. The generation planning sensitivity for the Holyrood CT was updated to 10 % since the last report for system planning purposes.

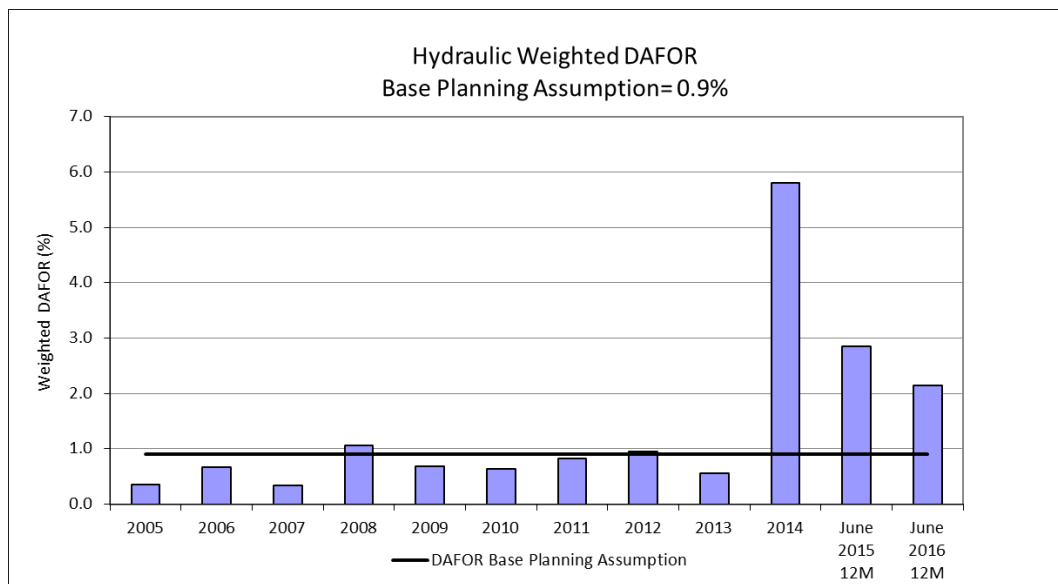
1 **4.0 Hydraulic Unit Forced Outage Rate Performance**

2

3 The hydraulic unit forced outage rates are measured using the CEA metric, DAFOR. Detailed
 4 results for the 12-month period ending June 30, 2016 are presented as well as the data for
 5 the 12-month period ending June 30, 2015. These are compared to Hydro’s generation
 6 planning assumption for the forced outage rate.

Generating Unit	Maximum Continuous Unit Rating (MW)	12 months ending June 2015 (%)	12 months ending June 2016 (%)	Hydro Generation Base Planning Assumption (%)
All Hydraulic Units - weighted	954.4	2.85	2.15	0.90
Hydraulic Units				
Bay D'Espoir 1	76.5	13.75	17.69	0.90
Bay D'Espoir 2	76.5	0.00	7.44	0.90
Bay D'Espoir 3	76.5	0.00	0.00	0.90
Bay D'Espoir 4	76.5	0.23	0.11	0.90
Bay D'Espoir 5	76.5	0.00	3.36	0.90
Bay D'Espoir 6	76.5	15.39	0.00	0.90
Bay D'Espoir 7	154.4	0.84	0.00	0.90
Hinds Lake	75	0.30	0.05	0.90
Upper Salmon	84	1.17	0.00	0.90
Granite Canal	40	0.37	1.83	0.90
Cat Arm 1	67	0.60	0.01	0.90
Cat Arm 2	67	1.91	0.21	0.90
Paradise River	8	0.00	0.31	0.90

7



1 Considering the individual units performance, the assumed Hydro generation base planning
2 DAFOR was materially exceeded for Bay d’Espoir Unit 1. Also, there were exceedances
3 compared to base planning assumption for Bay d’Espoir Unit 2, Bay d’Espoir Unit 5, and
4 Granite Canal for the current period.

5

6 The Bay d’Espoir Unit 1 DAFOR of 17.69% compared to the base planning assumption of
7 0.9% was the result of a forced extension of a planned outage. This one forced outage,
8 contributed 52% of the total DAFOR in this asset class. The planned annual maintenance was
9 scheduled from April 26, 2015 to May 15, 2015. The extension is the unanticipated result of
10 having to replace the turbine bearing. It was identified in the annual work plan to check the
11 turbine bearing clearances due to an increase in bearing temperatures. The bearing
12 clearances were checked and damage was found to the turbine bearing. Therefore it was
13 replaced with a new bearing. Vibration issues continued to be experienced at the unit after
14 the bearing was replaced, which extended the planned outage. Two vibration experts,
15 Hydro’s Project Execution and Technical Services personnel, as well as the Original
16 Equipment Manufacturer were retained to troubleshoot the issue, with the unit eventually
17 being returned to service at a reduced capacity. The original turbine bearing was reinstalled
18 after being refurbished (with reduced clearances) and, while the vibration issue remained, a
19 further dismantling of the unit revealed other issues including a damaged thrust bearing.
20 Additional repairs were made and a new thrust bearing installed, which resolved the
21 vibration issue, and the unit was returned to service at full capability on September 30,
22 2015. The Unit 1 DAFOR was also impacted (5.02%) by the Unit being removed from service
23 on May 21, 2016, as a result of a leak in Penstock 1, which provides water to both Units 1
24 and 2. The following detail relating to the Unit 2 DAFOR applies to Unit 1 as well.

25

26 The Bay d’Espoir Unit 2 DAFOR of 7.44% compared to the base planning assumption of 0.9%
27 was the result of a forced outage, caused by a leak in Penstock 1, which supplies both Units 1

1 and 2. The forced outage started on May 21, 2016 after a leak was reported in the Penstock.
2 A consultant was engaged to conduct an investigation into the issue, and a repair procedure
3 was provided on June 2. The damaged section of penstock was repaired and Unit 1 was
4 returned to service on June 3, 2016 at 1938 hours and Unit 2 was returned to service on
5 June 3, 2016 at 2014 hours.

6

7 The Bay d'Espoir Unit 5 DAFOR of 3.36% compared to the base planning assumption of 0.9%
8 was the result of a forced outage after the completion of planned annual maintenance. The
9 planned annual maintenance was completed from May 27, 2015 to August 7, 2015. Upon
10 starting the unit, a stator ground fault occurred, which required five days to repair before
11 the unit was placed into service on August 12, 2015.

12

13 The Granite Canal unit DAFOR of 1.83% compared to the base planning assumption of 0.9%
14 was the result of a forced outage after a lightning strike to transmission line TL263 which
15 connects the unit to the grid. A bearing issue (low water flow on the shaft seal) was
16 experienced on the restart of the unit. From August 10, 2015 to August 14, 2015, the unit
17 incurred forced unavailability while repairs were completed to resolve this issue. From
18 December 16, 2015 to December 17, 2015, the unit experienced forced unavailability due to
19 debris on the intake trash rack.

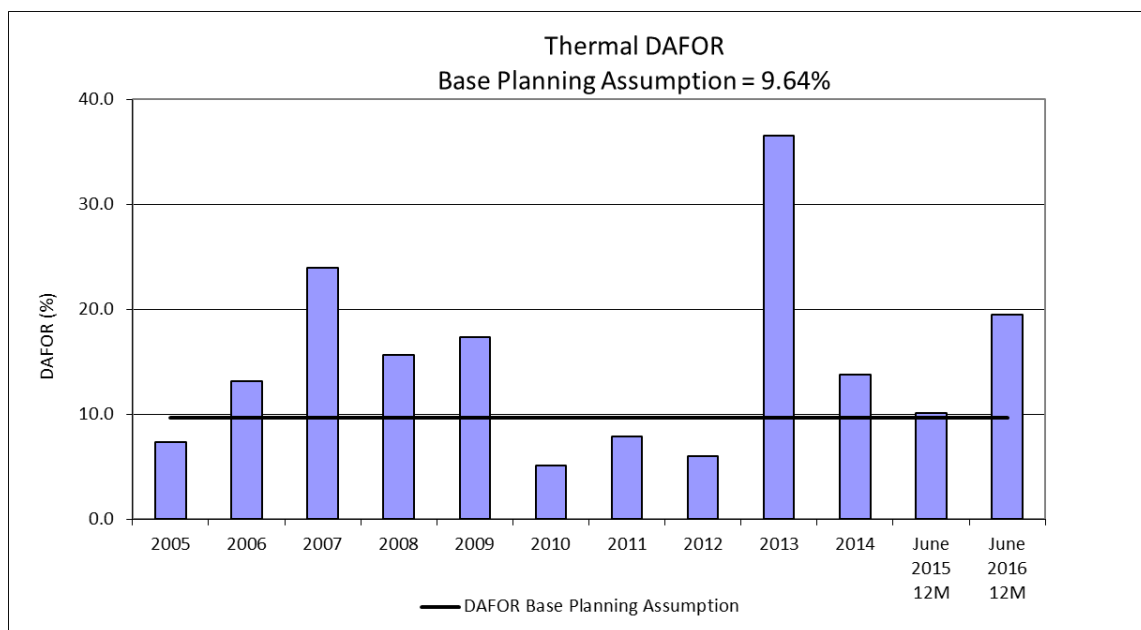
1 **5.0 Thermal Unit Forced Outage Rate Performance**

2

3 The thermal unit forced outage rates are measured using the CEA metric, DAFOR. Detailed
 4 results for the 12-month period ending June 30, 2016 are presented as well as the data for
 5 the 12-month period ending June 30, 2015. These are compared to Hydro’s generation base
 6 planning assumption for the forced outage rate.

7

Generating Unit	Maximum Continuous Unit Rating (MW)	12 months ending June 2015 (%)	12 months ending June 2016 (%)	Hydro Generation Base Planning Assumption (%)
<i>All Thermal Units - weighted</i>	490	10.06	19.45	9.64
Thermal Units				
Holyrood 1	170	13.20	20.66	9.64
Holyrood 2	170	11.06	26.46	9.64
Holyrood 3	150	5.67	8.91	9.64



8

9 For the 12-month period ending June 30, 2016 the weighted DAFOR for all thermal units of
 10 19.45% is above the assumed Hydro generation base planning DAFOR value of 9.64%, and
 11 also exceeded the previous 12-month period rate of 10.06%. Unit 1 DAFOR was 20.66% and

1 Unit 2 DAFOR was 26.46%, and the performance for both units was above the base planning
2 assumption of 9.64%. Unit 3 DAFOR was 8.91%, which is better than the base planning
3 assumption of 9.64%.

4
5 The DAFOR performance for Holyrood Unit 1 (170 MW) was affected by several events in the
6 current 12 MTD period.

7
8 From May 14, 2015 to August 1, 2015, a derating to 155 MW occurred due to airflow
9 limitations. During the 2015 planned maintenance outage from August to October, the
10 air heaters were found to be heavily fouled. They were cleaned during the outage. It was
11 expected that the air flow problem that led to the load restriction has been resolved as a
12 result of this clearing. Testing of the air flow controls during the maintenance outage did
13 not reveal any problems.

14
15 From November 27, 2015 to February 3, 2016 the unit was derated to 155 MW due to
16 airflow limitations, suspected to be related to the new variable frequency drives on the
17 forced draft (FD) fans. This was a continuation of the problems experienced prior to the
18 annual maintenance outage. The air heater fouling that was discovered and corrected
19 during the outage did not solve the problem with air flow. Boiler tuning may be effective
20 in resolving this issue. This is not possible to complete until after the reheater tubes are
21 replaced (see below).

22
23 On February 3, 2016 the east FD fan variable frequency drive failed and caused the unit
24 to trip. Investigation by Siemens (the manufacturer of the drives) and plant engineering
25 was conducted. Under a Siemens recommendation, a control card on the drive unit was
26 replaced and the unit was returned to service on February 5, 2016. When the unit was
27 returned to service the load was limited to 140 MW to make the unit more reliable in
28 consideration of the boiler reheater tube failures experienced in Unit 2. Siemens has

1 been actioned to complete a holistic investigation of all VFD issues that have occurred at
2 Holyrood. This was completed and presented to Hydro on July 7, 2016.

3
4 On February 8, 2016 the unit experienced a tube failure in the reheater section of the
5 boiler. The unit was operated with a deration to 50 MW until an opportune time to shut
6 it down for repairs was presented on February 16, 2016. Hydro considered the risk of
7 additional tube failures and the favorable weather forecast at the time and proceeded
8 with the replacement of the lowest wall thickness tubes during this outage. Sixteen
9 lower reheater tubes were replaced at that time. The unit was returned to service on
10 February 26, 2016 with a derating to 120 MW to improve the reliability of the reheater
11 until the remaining lower reheater tubes can be replaced during the upcoming scheduled
12 annual maintenance outage.

13
14 The DAFOR performance for Holyrood Unit 2 (170 MW) was primarily affected by several
15 events.

16
17 On January 6, 2016 the unit experienced a tube failure in the reheater section of the
18 boiler. Upon discovery of the failure the unit was taken offline in a controlled shutdown
19 and allowed to cool for internal inspection. Four failed tubes in the lower section of the
20 reheater were identified and replaced. The unit was returned to service after the repairs
21 on January 15, 2016. As is common practice when returning the unit to service, a
22 stepped approach to loading the unit was employed. Between January 15 and January
23 19, the unit was gradually loaded in steps between 70 MW and 140 MW. On January 19,
24 2016, when operating at 140 MW, the unit experienced another failure in the lower
25 reheater section of the boiler. Again the unit was taken offline in a controlled shutdown.
26 Hydro considered the risk of additional tube failures and the favorable weather forecast
27 at the time and proceeded with the replacement of the lowest wall thickness tubes
28 during this outage. Over the period since the unit first went out of service January 6,
29 2016, 27 lower and three upper reheat tubes were replaced prior to the unit going back

1 in service February 3, 2016. The unit was returned to service with a derating to 120 MW
2 to improve the reliability of the reheater until the remaining lower reheater tubes can be
3 replaced during the upcoming scheduled annual maintenance outage.

4
5 On May 26, 2016 the west FD fan variable frequency drive failed and caused the unit to
6 trip. Siemens (the manufacturer of the drives) was contacted immediately and a
7 technician was dispatched to travel to site. He did not arrive until late in the day on May
8 27, 2016. In parallel, the plant Electrical Engineer (in consultation with Siemens),
9 Electricians, and Operations conducted an internal investigation and determined that
10 there were no current faults with the fan and it could be safely started. It was decided to
11 put the unit back on line later in the day on May 26, 2016 while waiting for the Siemens
12 technician. Because the reason for the trip had not been determined, the unit load was
13 restricted to 50 MW (below UFLS).

14
15 The Siemens technician performed some on-line diagnostics on May 27, 2016 and May
16 28, 2016. Overnight on May 28, 2016 the unit was taken offline for a full internal
17 inspection of the drive under direction of the Siemens technician. A control card on the
18 drive unit was replaced and the unit was returned to service the next morning on May
19 29, 2016. Siemens has been actioned to complete a holistic investigation of all VFD issues
20 that have occurred at Holyrood since the drives were installed. This was completed and
21 presented to Hydro on July 7, 2016.

22
23 On June 20, 2016 the annual maintenance outage began on this unit. Included in the
24 scheduled work is the replacement of the lower reheater tubes.

1 **6.0 Gas Turbine UFOP Performance**

2

3 The combined UFOP for the Hardwoods, Happy Valley and Stephenville gas turbines was
 4 5.54% for the 12-month period ending June 30, 2016. This is better than the base planning
 5 assumption of 10.62%. The current period UFOP improved from the previous period UFOP of
 6 21.19%. The Hardwoods UFOP for the current period is 1.84%, which is better than the base
 7 planning assumption of 10.62%. The Stephenville unit’s current period UFOP is 3.59%
 8 compared to that of the previous period of 16.40%. Happy Valley’s UFOP is 14.04% for the
 9 current period compared to 1.03% in the previous period.

Gas Turbine Units	Maximum Continuous Unit Rating (MW)	12 months ending June 2015 (%)	12 months ending June 2016 (%)	Hydro Generation Base Planning Assumption (%)
<i>Combined Gas Turbines</i>	125	21.19	5.54	10.62
Stephenville	50	16.40	3.59	10.62
Hardwoods	50	32.44	1.84	10.62
Happy Valley	25	1.03	14.04	10.62

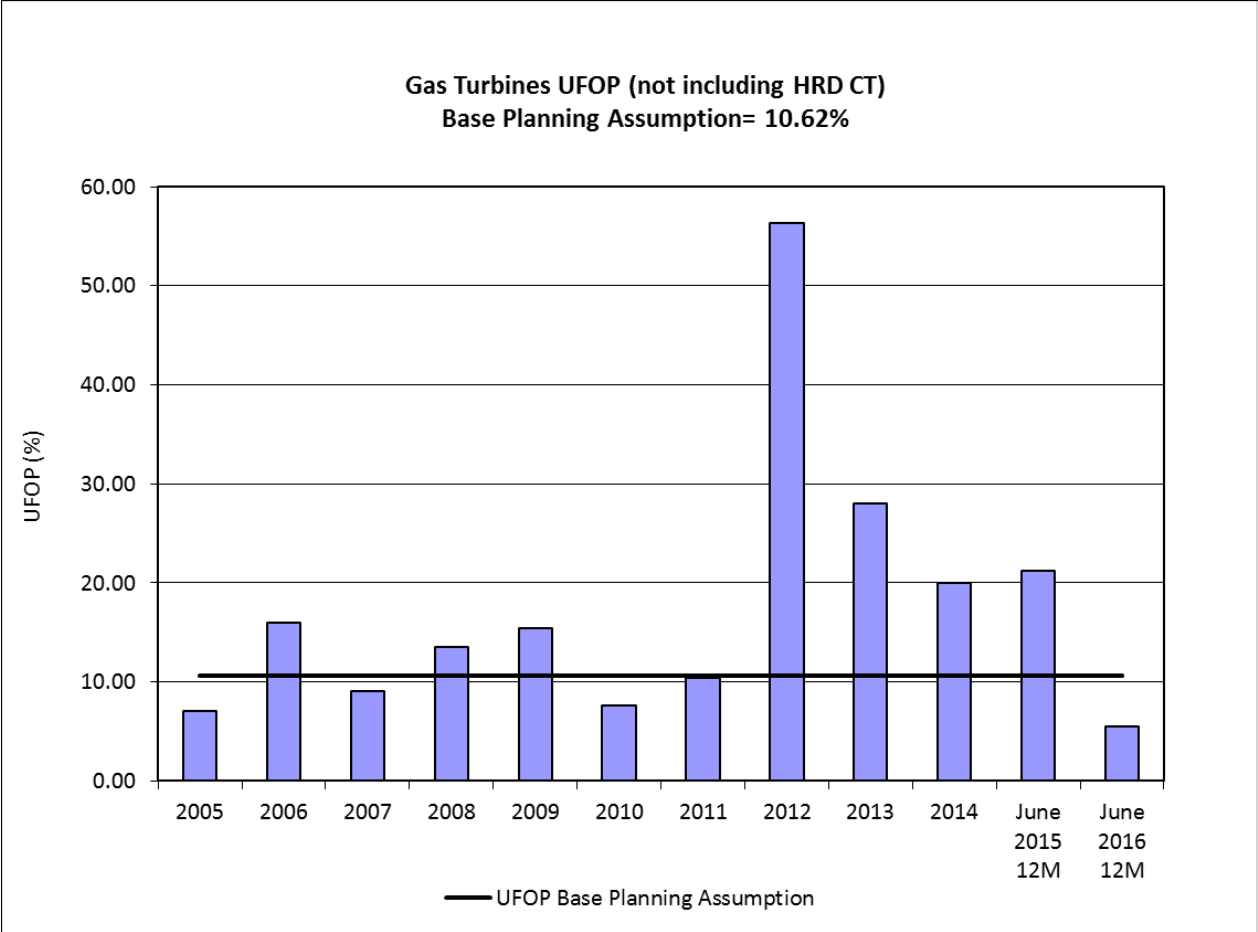
10

11 The Holyrood (HRD) CT UFOP of 2.53% for the current period is better than the base
 12 planning assumption of 5.00%.

13

14

Combustion Turbine Units	Maximum Continuous Unit Rating (MW)	12 months ending June 2015 (%)	12 months ending June 2016 (%)	Hydro Generation Base Planning Assumption (%)
Holyrood CT	123.5	1.56	2.53	5.00



- 1
- 2 The UFOP for the Happy Valley gas turbine was impacted by a forced outage from
- 3 September 9 to September 21, 2015 due to a vibration issue. The vibration issue was
- 4 determined to be a result of a broken air pipe which was repaired and the unit was then
- 5 tested and returned to service.